Journal of Thermal Analysis and Calorimetry, Vol. 62 (2000) 211–225

# Al–Ga–Zn PHASE DIAGRAM Calorimetric study of the isobaric invariants

## E. Aragon, K. Jardet, P. Satre and A. Sebaoun\*

Laboratoire de Physico-Chimie du Matériau et du Milieu Marin, Matériaux à Finalité Spécifique (E.A. 1356), Université de Toulon et du Var, B.P. 132, 83957 La Garde Cedex, France

(Received October 18, 1999)

### Abstract

The Al–Ga–Zn ternary phase diagram presents two isobaric invariant reactions: a eutectic at  $23\pm1^{\circ}$ C and a metatectic at  $123\pm1^{\circ}$ C [1–3]. Calorimetric measurements on the two isobaric invariant reactions have been carried out. First the Tammann method has enabled us to determine the composition of their limits on five isopletic cross sections. Then, the compositions of the invariant phases have been determined.

Keywords: calorimetric measurements, phase diagram, Tammann's method, ternary system Al–Ga–Zn

## Introduction

In previously published papers [1–2], we have proposed an Al–Ga–Zn phase diagram (Figs 1 and 2). In those papers, the stability fields of the phases in equilibrium as well as the ternary isobaric invariants have been determined. Studies have been carried out by the isopleth cutting method by using coupled direct and differential thermal analysis, X-ray diffraction at various temperatures and electron probe microanalysis. Six isopletic cross sections had been established. On these isopletic cross sections, two isobaric invariant reactions had been observed:

– A ternary eutectic:	$Ga_{SS} + Zn_{SS} + \alpha_{SS} \Leftrightarrow L_E$	$\Delta H_{\rm E} > 0$
- A ternary metatectic:	$Zn_{SS} + \alpha_{SS} + L_M \Leftrightarrow \alpha'_{SS}$	$\Delta H_{\rm M} > 0$

The temperatures of these two ternary invariant reactions  $(23\pm1^{\circ}C \text{ and } 123\pm1^{\circ}C, \text{ respectively})$  have been determined on heating by calorimetric measurements.

1418–2874/2000/ \$ 5.00 © 2000 Akadémiai Kiadó, Budapest Akadémiai Kiadó, Budapest Kluwer Academic Publishers, Dordrecht

<sup>\*</sup> Author for correspondence: Phone: 33-4-94-14-23-05; fax: 33-4-94-14-23-42; E-mail: sebaoun@univ-tln.fr



Fig. 1 Al-Ga-Zn diagram: monovariant lines and ternary invariant reactions



Fig. 2 Al-Ga-Zn diagram: reaction scheme

First, they enabled us to determine the limits of the invariant triangles on each isopletic cross section and then, to determine that triangles at the two invariant temperatures.

### Theoretical approach: the Tammann method

A well-known method for determining the composition of the binary invariant point has been established by Tammann at the beginning of the century [4–6]. This method has been widely used on the binary invariant reactions but concerning its application to ternary phase diagrams only few bibliographic data are available. The method has been described for few particular and theoretical cases of ternary systems [7]. However, rare works have been experimentally performed on that topic. In 1911, Loebe

[8] has presented twelve isopletic cross sections in the  $Pb_6Sb$ -Sn ternary system and the evolutions of the enthalpies associated with the invariant reactions have been followed on these sections. Tammann *et al.* [9] in 1925 have applied the method to the quasi-binary section Pb–Zn<sub>3</sub>Sb<sub>2</sub> in the Pb–Sb–Zn ternary system for determining the composition of the eutectic point on this section. In 1984, Tenu and Counioux [10] proposed a quantitative method which consists in measuring the enthalpies associated with the ternary invariant reaction for several compositions and to deduce from these measurements the composition of the eutectic point using the less square method. The precision of these method depends on the experimental parameters, particularly the heating rate.

Legendre *et al.* [11] have applied that qualitative method to the ternary system Au–Sb–Si. A similar method, applied to binary alloys of energetic materials, has been developed by Zi–Ru Liu *et al.* [12] and extended to ternary alloys [13] in order to determine the eutectic composition.

The Tammann's diagrams are based on the proportional variation of the heat quantity as a function of the mass of the phase formed or decomposed during the invariant reaction. That evolution is linear if all the calorimetric values measured on samples having an identical mass, are given in the correct unit (J  $g^{-1}$ ) [for a representation in atomic% the heat of reaction would be in this case given in J mol<sup>-1</sup>], moreover, if the composition scale is represented in mass percent<sup>\*\*</sup> [14]. These general remarks are true in binary as well as in ternary phase diagrams on isopletic cross sections. As a consequence, for an invariant reaction (Fig. 3):



Fig. 3 Enthalpies evolution on isopletic cross sections in a ternary phase diagram

\*\* The composition will always be given in mass percent.

$$A + B + C \Leftrightarrow D \qquad \Delta H_{Inv} > 0$$

a linear evolution is observed on the particular EF isopletic cross section (Fig. 3) as, in the general case, on the GH isopletic cross section (Fig. 3).

## Experimental

The samples were prepared by weighing and melting pure Al, Zn and Ga (99.999%) in cast iron crucibles with an internal graphite coating under nitrogen atmosphere.

This experimental study has been carried out by using the isopletic cross sections method. Four main isopletic cross sections (Fig. 4) have been chosen: ZA7–Ga  $(m_{Al}/(m_{Al}+m_{Zn})=0.07)$ , ZA15–Ga, ZA20–Ga and ZA40–Ga. In addition, two isopletic cross sections have been partly studied in order to determine the limits of the isobaric ternary invariants in the Al-rich corner: ZA74–AGa52 and ZA88–AGa22 (Fig. 4).



Fig. 4 Al-Zn-Ga diagram: isopletic cross sections for the experimental study

A differential scanning calorimeter (DSC 92 – Setaram) has been used: it allows invariant calorimetric measurements and low temperatures investigations by cooling in liquid nitrogen. Crucibles in stainless steel sealed with copper joins were used to prevent zinc vaporization and alloys oxidation. The used temperature range was from -50 to  $550^{\circ}$ C. The thermal analysis curves have been recorded both on heating and cooling. A heating and cooling rate of  $5^{\circ}$ C min<sup>-1</sup> has been chosen. The enthalpic measurements have been carried out on heating. The accuracy of the enthalpic measurements obtained after calibration is about 10% for composition determination and  $\pm 1^{\circ}$ C for temperature one. Each composition on the different isopletic cross sections has been studied by three successive thermal cycles.

The method used for determining the compositions of the invariant phases is based on an interpolative and iterative process. The main limit condition ( $\Delta H_{lnv}=0$ ) is verified on the limits of the invariant reaction. On the other hand, the  $\Delta H_{lnv}$  value is maximal at the invariant point (eutectic liquid  $L_E$  or  $\alpha'_{SS}$  metatectic phase). For any composition concerned by the invariant reaction, the  $\Delta H_{lnv}$  value is proportional to the quantity of the invariant phase formed on heating. This quantity is given by a barycentric relation at the end of the invariant reaction which corresponds to an indifferent equilibrium.

### Results

#### Temperatures of the stable and metastable invariant equilibria

The two isobaric invariant reactions have been identified on heating at  $23\pm1^{\circ}$ C for the ternary eutectic and at  $123\pm1^{\circ}$ C for the ternary metatectic.

 Table 1
 Al-Ga-Zn diagram: invariant temperatures (heating and cooling) and enthalpies (on heating) as a function of alloys composition on the ZA74-AGa52 isopletic cross section

Mass percent of gallium on the isopletic cross section ZA74–AGa52			10	15	20	25	30	35	40	45
	A /°C	heating			123	122	123			
Metatectic	U <sub>inv</sub> / C	cooling			103	102	103			
	Enthalpie	$es/J g^{-1}$			1.8	1.2	0.5			
Futactia	$\theta_{inv}/^{\circ}C$	heating		23	23	22	23	24	23	23
Eulectic	Enthalpio	es/J g <sup>-1</sup>		3.1	6.8	10.2	14.8	16.4	22	25.7

 Table 2 Al-Ga-Zn diagram: invariant temperature(s) and enthalpies (on heating) as a function of alloys composition on the ZA88-AGa22 isopletic cross section

Mass percent of gallium on the isopletic cross section ZA88–AGa22			5	10	15	20
	A /°C	heating				
Metatectic	U <sub>inv</sub> / C	cooling				
	Enthalpies/J	$g^{-1}$				
Futactia	$\theta_{inv}/^{\circ}C$	heating			23	
Eulectic	Enthalpies/J	$g^{-1}$			0.5	

On cooling the boundaries of the three-phase region  $(Zn_{ss}+\alpha_{ss}+\alpha'_{ss})$  and the eutectic transformation are displaced towards lower temperatures. The metatectic reaction is measured at 102±1°C (Tables 1 to 6 and Fig. 5). The eutectic transformation is displaced from 23°C on heating to  $-3^{\circ}$ C on cooling. But thermal accidents are observed up to  $-30^{\circ}$ C on cooling depending on sample compositions (Table 4 and

	1											
Mass percent of gallium on the isopletic cross section ZA7–Ga		0	2	5	7.5	10	13.5	15	17.5	20	22.5	
0 /90	heating			123	123	123	124	123	124	122	124	
Metatectic	$\sigma_{inv}/C$	cooling			101	102	102	103	102	102	103	102
Enthalpie	$s/J g^{-1}$			1.1	3.0	5.0	5.6	5.6	6.0	5.2	4.7	
Easta ati a	$\theta_{inv}/^{o}C$	heating			23		23					
Eutectic Enthalpies/J $g^{-1}$				1.9		4.5						
Mass percent of gallium on the isopletic cross section ZA7–Ga		25	28	31	35	41	45	54	63	77	93	
	0 /00	heating	123	124	124	122	123	123	123	123		
Metatectic $\theta_{inv}/ 0$	$\Theta_{inv}/C$	cooling	101	101	102	102	102	102	103	102		
E	Enthalpie	$s/J g^{-1}$	4.8	4.7	4.3	4.0	3.6	2.5	2.2	1.3		
Eutoatia	$\theta_{inv}/^{o}C$	heating	23					23				
Eulectic	Enthalpie	$s/J g^{-1}$	17					33				

 Table 3 Al-Ga-Zn diagram: invariant temperatures (heating and cooling) and enthalpies (on heating) as a function of alloys composition on the ZA7-Ga isopletic cross section

Mass percent	of gallium of	on the	0	2.5	5	10	14.1	17.5	20	25	27.5
heating					123	123	122	123	124	124	122
Metatectic	$\theta_{inv}/^{o}C$	cooling			102	102	101	102	102	102	102
Enthalpie	s/J g <sup>-1</sup>			0.1	4.3	7.7	9.5	9.5	8.2	8.0	
	Linnapie	heating			23	22	22	24	23	23	23
	$\theta_{inv}/^{\circ}C$	0			-3	-3	-3	-3	-2	-2	-3
Eutectic		cooling				-17	-5	-19	-3	-14	-12
	Enthalpies/J g <sup>-1</sup>				1.7	3.3	6.8	9.4	13	17	23
Mass percent isopletic cros	of gallium of s section ZA	on the 15–Ga	30	40	50	55	60	70	80	90	95
	A /°C	heating	123	123	124	122	123	123			
Metatectic	$\sigma_{inv}$ C	cooling	101	102	102	102	102	103			
Enthal		$s/J g^{-1}$	10.4	8.1	5.8	4.8	3.9	2.0			
$\theta_i$ Eutectic		heating	24	22	23	23	24	23	24	23	23
	$\theta_{inv}/^{\circ}C$	1:	-2	-3	-4	-3	-4	_4	-4	-3	-2
		cooling	-10	-9	-21	-12	-19	-17	-30	-24	-21
	Enthalpie	$s/J g^{-1}$	24	30	39	44	51	57	67	78	82

Table 4 Al-Ga-Zn diagram: invariant temperatures (heating and cooling) and enthalpies (on heating) as a function of alloys composition on theZA15-Ga isopletic cross section

21120	Gu isopiet									
Mass percent isopletic cros	Mass percent of gallium on the sopletic cross section ZA20–Ga		0	5.3	11	17	21	25.5	27.3	32
	0 /00	heating			122		123	124	122	123
Metatectic	$\sigma_{inv}/C$	cooling			102	102	102	103	102	101
	Enthalpie	$s/J g^{-1}$			3.0	7.0	9.1	9.5	10.3	8.5
E	$\theta_{inv}/^{o}C$	heating			23	22		24		
Eutectic	Enthalpie	$s/J g^{-1}$			3.4	8.1		15		
Mass percent isopletic cros	of gallium of s section ZA	on the A20–Ga	41	51	59	67	75	82	90	95.5
	0 /90	heating	123	123	124	122	123			
Metatectic	Oinv/ C	cooling	102	102	102	103	103			
	Enthalpie	$s/J g^{-1}$	7.2	5.1	4.0	1.9	0.5			
Eutoatia	$\theta_{inv}/^{o}C$	heating	23	24						
Eutectic Enthalp		$s/J g^{-1}$	26	34						

 Table 5 Al-Ga-Zn diagram: invariant temperatures (heating and cooling) and enthalpies (on heating) as a function of alloys composition on the ZA20-Ga isopletic cross section

	0										
Mass percent of gallium on the isopletic cross section ZA40–Ga		0	5	10	12	15	20	22	23	25	
	0 /00					123	122	123	122	122	122
Metatectic	$\sigma_{inv}/C$	cooling				103	103	102	101	101	101
	Enthalpie	$s/J g^{-1}$				1.3	2.3	4.0	5.2	5.1	5.1
Mass percent isopletic cros	of gallium of section ZA	on the 40–Ga	27	30	35	37.5	40	42.5	50	60	70
	A. /°C	heating	122	123	123	122	121	123	123	122	123
Metatectic	U <sub>INV</sub> / C	cooling	102	101	101	102	101	102	102	103	101
Enthalpies/J g <sup>-1</sup>		5.3	5.0	4.3	4.1	4.0	3.9	2.7	1.28	0.4	

Table 6 Al-Ga-Zn diagram: invariant temperatures (	(heating and cooling) and enth	nalpies (on heating) as a functi	on of alloys composition on the
ZA20-Ga isopletic cross section			

ARAGON et al.: TERNARY SYSTEM Al-Ga-Zn

Fig. 5b). These accidents seem to correspond to the crystallization of two allotropic forms of gallium which are metastable at the atmospheric pressure [15–17]. As a consequence, a liquid phase appears at 23°C on heating and can stay present on cooling up to  $-30^{\circ}$ C for some alloys.

#### Enthalpic measurements on the isopletic cross sections

Enthalpic measurements have been carried out on the four main isopletic cross sections and for the two invariant reactions (Tables 1 to 6).

The metatectic reaction has been studied in order to determine the composition of the invariant phases. For that, the limits of the metatectic invariant (compositions



Fig. 5a Al-Ga-Zn diagram: ZA7-Ga isopletic cross section



Fig. 5b Al-Ga-Zn diagram: ZA15-Ga isopletic cross section



of the  $A_i$  and  $C_i$  points: Fig. 5) have been previously determined on each cross section by using the Tammann method. The compositions of the points  $B_i$  have also been de-

Fig. 5c Al-Ga-Zn diagram: ZA20-Ga isopletic cross section







Fig. 5e Al-Ga-Zn diagram: ZA74-AGa52 isopletic cross section

termined (Fig. 5). The accuracy for the determination of  $C_i$  is better than the determination of  $A_i$  because of a larger composition gap between  $B_i$  and  $C_i$  than between  $A_i$ and  $B_i$ . The determination of the points  $A_5$  and  $B_5$  on the ZA74–AGa52 isopletic cross section have not been possible for this reason. On the ZA15–Ga isopletic cross section (Fig. 5-b), between 19 and about 29% of gallium, the enthalpic values are similar and do not show a linear change.

This behaviour is due to the nearness of the metatectic point (Fig. 6a) which is confirmed by the highest enthalpic values measured for these compositions. In fact, two different maxima ( $B_2$  and  $D_2$ ) are observed on that cross section. The composition of  $B_2$  can be determined with a correct accuracy: it corresponds to the composition for which the enthalpic values become almost constant (between 17.5 and 20%: Table 4). Using the same reasoning, the composition of  $D_2$  seems to be below 30%. But Fig. 6a shows that the ZA15–Ga isopleth is nearly parallel to the ( $M-L_M$ ) tie-line on which  $D_2$  is located. The composition of  $D_2$  is therefore very difficult to determine. The compositions of the  $A_i$ ,  $B_i$  and  $C_i$  points are given in Table 7.

 Table 7 Compositions (mass% Ga) of the limits of the metatectic reaction on the studied isopletic cross sections

ZA7	–Ga	ZA1	5–Ga	ZA2	0–Ga	ZA4	0–Ga	ZA74	AGa52
$A_1$	4	$A_2$	7	$A_3$	8	$A_4$	11	$A_5$	_
$\mathbf{B}_1$	11	$\begin{array}{c} B_2 \\ D_2 \end{array}$	19 ≈29	$B_3$	23	$B_4$	24	$B_5$	_
C1	76	C <sub>2</sub>	79	C <sub>3</sub>	78	$C_4$	72	C <sub>5</sub>	33

On the other hand, the limits of the eutectic reaction have also been studied. Because of the composition of the eutectic point (about 95% [18]), a linear change of the enthalpic values is observed on a large field of compositions. Our measurements do not allow to precise the equilibria in the Ga-rich corner. Then, the  $A'_i$  points have only been determined but with a good accuracy because the isopletic cross sections intersect perpendicular to the iso-enthalpic lines (Fig. 5). Their compositions are given in Table 8:

 Table 8 Compositions (mass% Ga) of the limits of the eutectic reaction on the studied isopletic cross sections

ZA7	–Ga	ZA15	5–Ga	ZA20	)–Ga	ZA74-	-AGa52
$A'_1$	3	$A'_2$	4	$A'_3$	5	$A'_5$	12

#### Determination of the composition of phases for the invariant reactions

Using the  $A_i$ ,  $B_i$  and  $C_i$  positions, the compositions of the metatectic invariant phases have been determined. The determination of the composition of the  $\alpha_{ss}$  metatectic phase is the more accurate: it corresponds to the intersection point between the three  $(A_1-A_2-A_3-A_4-A_5)$ ,  $(B_3-B_4)$  and  $(C_2-C_3-C_4-C_5)$  straight lines. The compositions of the other phases participating to the metatectic reaction are determined identically.



Fig. 6a Al-Ga-Zn diagram: isobaric eutectic at 23°C



Fig. 6b Al-Ga-Zn diagram: isobaric eutectic at 123°C

Less information is available for determining the eutectic invariant phases. The  $\alpha_{ss}$  eutectic phase is located on the  $(A'_1-A'_2-A'_3-A'_5)$  well defined straight line which allows to determine its gallium composition. The enthalpic measurement obtained on the ZA88–AGa22 isopletic cross section (Table 2) allowed to conclude that its zinc composition is lower than 5% and a more in-depth analysis of the enthalpic data obtained on the ZA74–AGa52 isopletic cross section (Table 2 and Fig. 5e) conducts to the composition given in Table 9. The composition of Zn<sub>ss</sub> phase for the metatectic reaction is also determined with a low uncertainty. Some thermal analysis experiments

conducted in the Ga-rich corner have allowed us to confirm the compositions of the eutectic Ga<sub>ss</sub> and liquid phases given by Ansara [18].

The composition of the invariant phases determined by the Tammann method are summarized in Table 9.

The gallium solubility in the  $\alpha_{ss}$  ternary solid solution at 23°C (about 14% – Fig. 6a) is lower than those in the  $\alpha_{ss}$  binary solid solution (about 20%) given at 26°C [19]. Moreover, that miscibility evolves from 14% at 23°C to 20% at 123°C (Fig. 6b) in the ternary diagram. On the other hand, the miscibility of zinc seems to be approximately constant and at a low value (about 5%).

 Table 9
 Al-Ga-Zn diagram: isobaric invariant equilibria – composition of the invariant phases

T	DI	Co	Composition/mass%±2%					
Type	Phases	Al	Zn	Ga				
Metatectic	L <sub>M</sub>	≈2	18	80				
	$\alpha_{\rm SS}$	72	8	20				
	$\alpha'_{ss}$	13	66	21				
	Zn <sub>SS</sub>	2	94	4				
Eutectic	$L_{E}$	≈3	≈3	≈94				
	$\alpha_{\rm SS}$	84	2	14				
	Zn <sub>SS</sub>	≈1	97	2				
	Ga <sub>SS</sub>	≈2	≈2	≈96				

#### Conclusions

This study allowed to confirm the composition of invariant phases and temperature for the eutectic-type isobaric invariant obtained by modelling from the three binary of the bibliography.

Concerning the metatectic isobaric invariant observed at 123°C, it does not agree with the first class peritectic one proposed by bibliography at 282°C [18]. We have determined the composition of the invariant phases.

\* \* \*

The authors thank the D.G.A./D.C.N. (Délégation Générale de l'Armement/Direction des Constructions Navales) of Toulon for financial support during the thesis preparation of E. Aragon at Toulon University. In particular, the help of Mr. Giroud is gratefully acknowledged.

### References

- 1 E. Aragon, K. Jardet, P. Satre and A. Sebaoun, Al–Zn–Ga phase diagram: Part I, J. Therm. Anal. Cal., 53 (1998) 769.
- 2 E. Aragon, K. Jardet, P. Satre and A. Sebaoun, Al–Zn–Ga phase diagram: Part II, J. Therm. Anal. Cal., 53 (1998) 785.

224

- 3 E. Aragon, Thesis, Toulon University, France (1995).
- 4 G. Tammann, Z. Phys. Chem., 37 (1903) 303.
- 5 G. Tammann, Z. Phys. Chem., 45 (1905) 24.
- 6 G. Tammann, Z. Phys. Chem., 47 (1905) 289.
- 7 M. Sahmen and A. V. Vegesack, Z. Phys. Chem., 59 (1907) 257.
- 8 V. R. Loebe, Metallurgie, 8 (1911) 7.
- 9 G. Tammann and O. Dahl, Z. Anorg. U. All. Chem., 144 (1925) 1.
- 10 R. Tenu and J. J. Counioux, Communication aux J.E.E.P., Tours (1984).
- 11 B. Legendre and Chay Hancheng, Bull. Soc. Chim. Fr., 2 (1986) 138.
- 12 Zi-Ru Liu, Ying-Hui Shao, Cui-mei Yin and Yang-Hui Kong, Thermochim. Acta, 250 (1995) 65.
- 13 Cui-mei Yin, Zi-Ru Liu, Ying-Hui Shao and Yang-Hui Kong, Thermochim. Acta, 250 (1995) 77.
- 14 A. P. Rollet and R. Bouaziz, L'Analyse Thermique (tome 1), Gauthier Villars ed., Paris 1972.
- 15 A. Defrain, I. Epelboin and M. Erny, C.R.A.S., 250 (1960) 2553.
- 16 A. Defrain and I. Epelboin, C.R.A.S., 249 (1959) 50.
- 17 P. W. Bridgman, Phys. Rev., 48 (1935) 893.
- 18 I. Ansara, G. Petzow and G. Effenberg ed., Ternary Alloys, 5 (1991) 552.
- 19 T. B. Massalski, Binary Alloy Phase Diagrams (2nd Edition), B. Massalski ed., 1992.